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FORCE AND MOMENT MEASUREMENTS ON A 74° DELTA WING WITH AN APEX FLAP (Data Report)

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## **ABSTRACT**

Results are presented of a subsonic experimental investigation of an apex flap concept on a 74° swept delta wing with trailing-edge flaps. The apex flap comprised approximately 6 percent of the wing area forward of a transverse hinge, allowing for both upward and downward deflection angles from +40° to -20°. Upward deflection forces leading-edge vortex formation on the apex flap, resulting in an increased lift component on the apex area. The associated nose-up moment balances the nose-down moment due to trailing-edge flaps, resulting in sizeable increase in the trimmed lift coefficient particularly at low angles of attack. Nose-down apex deflection may be used to augment the pitch control for rapid recovery from high-alpha maneuvers. Balance measurements were obtained in the NASA Langley 7- by 10-Foot High-Speed Tunnel at  $M_{\infty} = 0.2$  and  $R_{\overline{c}} = 4 \times 10^{\circ}$ . This report presents the balance data without analysis.

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# LIST OF SYMBOLS

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α, ALPHA angle of attack, deg
           wing span, cm
β, BETA
           sideslip angle, deg
Ē
           mean geometric chord, cm
CA
           axial-force coefficient, Axial force/q_S
CD
           drag coefficient, Drag/q_S
CL
           lift coefficient, Lift/q_S
CMS
           pitching-moment coefficient, Pitching moment/q_Sc
CN
           normal-force coefficient, Normal force/q_S
           upper surface pressure coefficient, (P_u - P_{\infty})/q_{\infty}
C_{DU}
C_{\mathbf{r}}
           wing root chord, cm
CRMS
           rolling-moment coefficient, Rolling moment/q_Sb
           side-force coefficient, Side force/q_{\infty}S
CYS
           yawing-moment coefficient, Yawing moment/q_{\infty}Sb
CYMS
D
           drag, N
           apex flap deflection, deg
δa
           trailing-edge flap deflection, deg
\delta_{\mathsf{TF}}
L
           lift, N
LE
           leading edge
M
           free-stream Mach number
P1,
           upper surface static pressure, Pa
P‱
           free-stream static pressure, Pa
Q,q_{\infty}
           free-stream dynamic pressure, Pa
R<sub>z</sub>
           free-stream Reynolds number based on \bar{c}
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S wing planform area, cm<sup>2</sup>

 $X/C_r$  x-location in fraction of root chord

#### INTRODUCTION

Supersonic aircraft configurations generally utilize thin, highly swept wings of delta or related planform primarily for their supersonic and high subsonic aerodynamic qualities. In the supersonic regime, wave drag is reduced due to the small thickness ratio and high sweep angle. High drag-divergence Mach number is another advantage of the delta wing in high subsonic and transonic flight. However, the highly swept delta wing has certain deficiencies such as poor lift at low angles of attack and excessive drag at high lift coefficients.

Recent studies at NASA Langley Research Center and elsewhere have attempted to correct these disadvantages through vortical flow manipulation. This approach consists of devising means of reordering or relocating the leading-edge vortex system inherent to highly swept wings. References 1 and 2 report extensive studies of leading-edge devices used to enhance the low speed characteristics of a 60° delta wing by such vortex flow manipulation. However, those studies were directed toward improving the high-alpha characteristics of the delta; comparatively little has been done to improve its low-alpha lift capability which is important during take-off, landing and other low-speed, low-alpha maneuvers. One of the previous devices, the leading-edge vortex flap, has been tested in the up-deflected sense (ref. 3) to force an earlier formation and strengthening of the leading-edge vortex system to increase the lift at low-alpha. However, a large portion of the wing (e.g., 20 to 30 percent of the total area) had to be deflected to obtain even modest lift gains (i.e.,  $\Delta C_1 = 0.50$ ) on a 74° delta wing. Flaps of this size will pose actuation problems and severely reduce the usable volume in the wing.

In this investigation, the apex portion of the delta wing is hinged transversely and deflected upwards to induce vortex formation from its leading edges (fig. 1). With the vortex lift primarily concentrated in the apex region, a relatively small percentage of the wing area occupied by the apex flap should generate a substantial positive pitching moment. This moment may be used to trim out flow-augmented trailing-edge flaps to yield relatively high increments of usable lift. If the apex vortices persist in strength downstream on the main wing surface, an additional lift due to the induced suction effect may be obtained.

This report documents the force and moment data acquired in the NASA Langley 7- by 10-Foot High Speed Tunnel on a 74° planar delta wing incorporating an apex flap and trailing-edge flaps. The test model configurations included apex flap deflected upward, apex flap up plus trailing-edge flaps down, and differential trailing-edge flaps as elevons. Some configurations were also tested in sideslip. The tabulated force data are presented without analysis.

#### RESEARCH MODEL

The model used in this study is constructed from aluminum and has a root chord length of 40 inches. The leading edges as well as the trailing edge are symmetrically bevelled. The apex flap was obtained by incorporating a transverse hinge at  $\text{X/C}_r = 0.25$ . The force model was also fitted with hinged trailing-edge flaps (see fig. 2 for dimensions) capable of independent deflection in both the upward and downward direction. The hinge lines were taped to prevent leakage. A six-component sting-type balance (NASA Model 738) was housed in a streamlined fuselage provided for this purpose. See figure 2 for model dimensions and planform characteristics.

#### WIND TUNNEL FACILITY

NASA Langley Research Center's 7- by 10-Foot High-Speed Tunnel is a continuous-flow, closed circuit, subsonic-transonic tunnel which operates at ambient atmospheric conditions. The test section of the tunnel is 6.59 feet high and 9.58 feet wide, with a usable length of 10.28 feet.

The model support system used in this test is referred to as the standard angle-of-attack sting. It consists of a vertical strut with a variable pitch angle sting support system with a range of approximately -4° to 20°. In addition to the pitch mode, the standard sting has a vertical translation mode which allows the model to be kept near the center of the test section throughout the angle-of-attack range. Reference 4 contains a detailed description of the tunnel facility.

The data acquisition, display, and control system for the 7- by 10-Foot High-Speed Tunnel is controlled by a dedicated on-site computer. The system includes a Xerox Sigma-3 computer, a data acquisition unit, a line printer, and a Tektronix 4014 graphics terminal. Reference 5 contains a detailed description of the data reduction capabilities of the system.

# DATA REDUCTION

Forces and moments as sensed by a wind tunnel balance must be corrected for external interferences unrealistic of actual flight. Jet boundary corrections were applied to the angle of attack to account for the vertical flow component induced by the walls at the model (ref. 6).

To account for initial balance loads due to model weight, "wind-off" weight tare measurements were taken at various balance attitudes and used in the reduction of balance data (ref. 7). Balance axial force measurements were corrected for housing pressure drag by using chamber (base) pressure measurements. The method of reference 7 was used to

calculate and correct for the solid and wake blockage effects. Since the angle of attack was measured by means of an accelerometer located inside the model, no correction for sting bending due to aerodynamic loading was necessary. Once all necessary corrections were applied to the force and moment data, the final results were presented in coefficient form.  $C_L$  and  $C_D$  are oriented along the conventional wind axis, with  $C_A$  and  $C_N$  (axial and normal force coefficients, respectively) along the body axis. Moments are calculated about the reference center shown in figure 2.

### DATA PRESENTATION

The tests were conducted at  $M_{\infty}=0.2$  and  $R_{\overline{c}}=4\times10^6$ . Apex up deflections ranged from 0° to 40° in 5° increments. Angle-of-attack range was -4° to 19.5°. Apex down deflections of -5°, -10°, and -20° were also tested.

Several "tandem" configurations, i.e., up-deflected apex together with down trailing-edge flaps, were also tested. Roll control effectiveness with the trailing-edge flaps deflected as elevons for positive rolling moment (fig. 3), as well as lateral/directional characteristics at  $\pm 5^{\circ}$  sideslip were also investigated.

The test data are presented without analysis. Table I provides a configuration summary for all force runs, and provides a key to the tabulated data listed by run number in Table II.

## REFERENCES

- 1. Tingas, S. A.; and Rao, D. M.: Subsonic Balance and Pressure Investigation of a 60-deg. Delta Wing with Leading-Edge Devices. NASA CR-165923, May 1982.
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- 3. Marchman, J. F.: The Aerodynamics of Inverted Leading Edge Flaps on Delta Wings. AIAA Paper No. 81-0356, 1981.
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- 5. Fox, C. H., Jr.: Real-Time Data Reduction Capabilities of the Langley 7- by 10-Foot High-Speed Tunnel. NASA TM 78801, 1980.
- 6. Gillis, C. L.; Polhamus, E. C.; and Gray, J. L., Jr.: Charts for Determining Jet-Boundary Corrections for Complete Models in 7- by 10-Foot Closed Rectangular Wind Tunnels. NACA NR L-123, 1945.
- 7. Herriot, J. G.: Blockage Corrections for Three-Dimensional-Flow Closed-Throat Wind Tunnels, with Consideration of the Effect of Compressibility. NACA Rep. 995, 1950.

TABLE I. RUN SUMMARY

Description	Run #	δ <sub>a</sub>	δ <sub>TE</sub> (L/R)	β (deg)
planar delta	1	0°	0/0	0
Apex	30 2,3	5° 10°	0/0 0/0	0
flap	31 4	15° 20°	0/0 0/0	0 0
deflection	51 5	25° 30°	0/0 0/0	0
only	52 6	35° 40°	0/0 0/0	0
Apex/T.E.	7 8	0° 0°	10/10 15/15	0
Flap	9 10	0°	20/20 25/25	0 0
Series	11 30 22 12 29 21 32 33 23 13 28 18 24 14,17 27 19 25 15,16 26 20	0° 5° 10° 10° 10° 15° 20° 20° 20° 30° 30° 30° 40° 40° 40° 40°	30/30 10/10 10/10 15/15 20/20 25/25 10/10 15/15 10/10 15/15 20/20 25/25 10/10 15/15 20/20 25/25 10/10 15/15 20/20 25/25	0 0 0 0 0 0 0 0 0 0

TABLE I. Concluded

Description	Run #	$^{\delta}$ a	<sup>δ</sup> TE (L/R)	β (deg)
Sideslip	36 37	0°	0/0 0/0	+5 -5
Tail-On	35	20°	0/0	-5 +5
Sideslip	59 50	0°	. 0/0	+5
Tail-Off	56 58	0° 20°	0/0 0/0	-5 +5
	57	20°	0/0	<b>-</b> 5
Negative	55	-5°	0/0	0
apex flap deflection	53 54	-10° -20°	0/0 0/0	0 0
Elevon	49	0°	+15/-15	Ō
configurations	50	20°	+15/-15	0

TABLE II. TEST RESULTS

	NASA LANGLEY					7 X 10 HIGH SPEED TUNNEL					
			TEST 10			RUN 1					
MACH	PA	ALPHA Deg	SETA DEG	CL	CD	CHS	CRMS	CYMS	CYS	CH	CA
.200 .200	2741.4	.01	00	.0095	.0073	.0037	0002 0001	.0009	0015	.0055	.0073
.200	2739.0 2745.4	-1.93 -4.16	.02	1084	.0150	0068	0003	.0008	0020	0435 1092	.0073
.200	2762. <b>6</b> 2756.7	.03 1.91	00 01	.0047 .0537	.0073 .0092	.0037	0005 0004	.0007	0018	.0047	.0073
.200	2753.3	3.92	02	.1120	.0147	.0163	0001	.0008	0018	.1120	.0070
.200	2743.8 2742.2	5.62 7.80	03 04	.1770	.0245	.0248	.0000	.0007	0024	.1786 .2536	.0061
.200	2750.7 2752.8	9.91 11.61	05	.3343	.0642	-0507	.0004	.0006	0021	.3404	.0057
• Z00	2762.8	13.87	06	.4991	-1280	.0641	.0004	.0008	0024	.4191 .5152	.0051
.201 .200	2787.5 2754.7	16.13 17.94	07 08	.6C24 .6G34	.1784 .2245	.1027 .1196	.0012	.0006	0016	.6283	.0040
.201	2766.0 2770.2	19.26	09	.7454	.2632 .0074	.1334	.0011	0001	0024 0031	.7905	.0026
			***	*****		******	******	,,	10071	*****	
			TEST 10	-		RUM 2					
MACH	PA	ALPHA Deg	BETA Deg	CF	CO.	. CMS	CRHS	CYMS	CYS	CH	CA
.201	2761.6	.03	00	.0094	.0097	.0094	0005	.0008	0012	.0094	.0097
.200 .201	2756.3 2760.6	-1.99 -4.36	.01 .02	0406 1128	.0110	.0027 0063	0006	.0009	0005 0021	0409 1137	.0095
.201	2771.9	.01	00	.0080	.0104	.0090	0004	.0008	0014	.0080	.0104
.201 .201	2762.2 2764.7	1.94	01 02	.0598	.0130 .0198	•0172 •0260	0001 .0001	.0012	0014 0013	.0602 .1101	.0110
.200	2757.1 2747.0	5.81 7.80	03	.1822	.0311	.0364	.000Z	.0008	0002	.1844	.0125
.200	2748.6	9.84	05	.3421	.0743	.0487 .0633	.0001	.0008	0016 0024	.2669 .3498	.0137 .0147
.200 .201	2745.5 2762.0	11.87 13.87	06	.4261 .5087	.1060 .1432	.0803	.0008	.0008	0012 0030	.4367	.0161
.200	2757.1	15.82	07	.5966	.1860	-1153	.0013	.000Z	0013	.5282 .6252	.0171
.201 .200	2762.9 2741.4	17.84 19.33	cs 09	.6866	.2411 .2871	.1342 .1506	.0014	0002	0026 0028	.7274 .8098	.0192
.201	2766.6	.01	70	.0105	.0098.	.0096	0004	.0006	0018	.0102	.0098
			TEST 10	<b>.</b>		RUM 3					
MACH	٥	ALPHA	BETA	CL	CD	CHS	CRMS	CYMS	CYS	CN	CA
NUMB	PA	DEG	DEG								_
.201 .200	2780.7 2764.7	.03 -4.32	00	.0084 1142	.0103 .0167	.0091	0004	.0010	0006 0016	.0084 1152	.0103
.200 .201	2764.5 2779.4	.01 3.88	00	.0075	.0105	.0092	0005 0001	.0010	0017	.0075	.0104
.199	2748.6	7.78	04	. 2396	.0502	.0484	.0004	.0012	0014 0026	.1160 .2640	.0121
.200 .201	2770.5 2783.5	11.82 15.79	05	.4182	.1045 .1674	.0789 .1151	.0007	.0006	0029 0014	.4307 .6215	.0166
.200	2774.2	19.49	09	.7642	.2927 .0105	.1523 .0094	0013	000Z	0026	.8180	.0210
*			•••	*****		*****	*****		-10012	•0072	.0103
			TEST 10	6		RUN 4					
MACH	۰	ALPHA	BETA	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
8MUM 005.	PA 2769.6	. DE6	⊅£.5 00	.0275	.0207	.0293	0008	.000#	001m	.0276	.0436
.200	2766.5 2785.9	-1.93 -4.12	.01	0468 1083	.0196	0009	0005	.0006	0019 0021	0494 1097	.0179
.201	2795.2	.08	00	.0265	.0207	. 0297	<b>→.</b> 0007	.0007	0013	.0266	.0207
.201	2786.8 2782.5	1.96 4.13	01 02	.0714	.0263 .0361	.0382	0005 0003	.0006	0021 0029	.0723 .1326	.0238
.200	2762.4	5.49	03	.1859	.0484	.0572	0003	.0006	0039	.1899	.0291
.200	2767.8 2770.4	7.88 9.92	04	.2632	8940. 4890.	.0701 .0838	0002	.0003	0012 0032	.2703 .3653	.0331
.200	2799.3	11.68	05	.4337	.1316	1001	.0007	.0000	0034	.4516	. 0397
.200	2780.9 2780.4	.08 9.91	00	.0258	.0207	.0294	0008 .0007	.0008	0011 0022	.3666	.0206
. 200	2780.3	11.88	05	.4316 .5194	.1311	.0996	.0008	.0000	0025	.4494	.0394
.199 .201	2754.2 2785.5	13.95 15.93	06 07	.6020	.1733 .2201	.1370	.0015	0010	0025 0026	.6393	.0464
.200	2765.8	17.95	00	.0405	.2786	41275	.0014	0014 0012	0031	.748Z .8245	.0505
.200	2776.3 2772.9	19.36	08	.7603 .0271	.0200	.1725 .0304	0005	.0006	0032	.0271	.0531
			TEST 10	6		RUN 5					
HACH	٥	ALPHA	BETA	Cr.	CD	CHS	CRHS	CYMS	CYS	CH	CA
NUMB .200	PA 2778.1	.12	.00	.0352	.0400	.0425	0014	.0000	0036	.0353	.0399
.200	2765.4	-1.84	.01	0395	.0360	.0263	0004	.0005	0028	0406	.0347
.200 .200	2767.7 2775.8	-4.07 .14	.02 .00	1067 .0356	.0381	.0102 .0425	0008	.0003 0001	0032	1092 .0357	.0304
.201	2784.3	2.15	01	.0942	.0498	.0589	0004	.0002	0030	.0960	.0463
.201 .200	2781.5 2773.4	4.07 5.97	02	.1476 .1992	.0613	.0707 .0795	0002	.0002 0002	0050 0048	.1516 .2059	.0507
.201	2782.2	7.93	03	. 2574	.0945	.0886	.0003	0022	0048	.2680	.0581
.200	2773.7 2785.1	9.97 11.92	04	.3373 .4164	.1233 .1573	.1000 .1126	.0005	0015 0018	0059	.3536 .4399	.0631
.200	2768.3	13.98	06	.9011	.2001	.1283	.0006	0018	0063	.5346	.0731
.201	2F01.7 2790.2	15.89	07 07	.5800	.2464	.1440	.0010	0022	0068	.6253 .7278	.0781
.202	2810.5	19.38	08	. 7243	.3473	.1766	.0012	0026	0082	.79±5 .0370	.0873
.200	2772.7	.11	.00	.0369	.0406	.0422	0005	5001	0049	.0370	.0406

			TEST 10			RUN 6					
MACH	q	ALPHA	ATSE	CL	CD	CHS	CRMS	CYMS	CYS	CN	CA
.201	PA 2786.5	0EG	.00	.0271	.0524	.0476	0005	0001	0042	.0273	.0523
.200 .200	2767.6 2769.4	-1.86 -4.01	.01	0302	.0496	.0329	.0000 0006	.0003	0039 0037	0318 0917	.0486
.200	2763.5	-11	.00	.0262	.0522	.0469	0002	.0000	0037	.0263	.0522
.201	2784.9 2770.9	2.03 4.06	01 02	.0912	.0594	.0599	0004 0001	0000	0038 0038	.0932 .1523	.0561 .0612
.200	2758.1 2775.4	5.93 7.91	02	.2004 .2645	.0865	.0796 .0893	.000z	0007 0007	0034 0037	.2083 .2768	.0654 .0704
.200	2778.2	9.97	04	.3371	.1368	.1011	.0005	0010	0040	.3557	.0764
.200 .201	2770.2 2787.7	11.92 13.95	05	.4063 .4853	.1696 .2104	•1125 •1253	.0009	0013 0016	0052 0058	.4345 .5217	.0816
.201	2705.7 2777.2	15.87 17.92	07 07	.5658 .6519	.2575 .3152	.1386 .1543	.0013	0021 0019	0051 0072	.6147 .7172	.0930
.201 .200	. 2780.0 2773.3	19.36	08	.7071	.3578 .0527	.1657 .0472	.0013	0025	0060	.7857	.1032 .0526
••••	2	•••		.0320	.0321	*****	10001	,,,,,,	-10030	.0321	
	•		TEST 10	6		RUM 7					
MACH	Q PA	ALPHA	BETA	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
.200	2777.1	.01	DE€ 00	.0493	.0099	0090	0011	.0005	0002	.0493	.0099
.200 .199	2776.8 2755.2	-1,95 -4,30	.01	0001 0642	.0098	0148 0235	0014 0014	.0006	0002 0012	0004	.0098
.200	2771.0 2789.3	.02 1.98	00 01	.0451 .1024	.0099	0091 0036	0011 0012	.0006	0010 0008	.1028	.0099
. 200	2779.4	3.91	02	.1621	.0212	.0028	0010	.0006	0010	.1631	.0101
.200	2768.4 2759.6	5.95 7.78	03 04	.2382	.0351	.0102 .0193	.0001	.0005	0013 0017	.2405 .3097	.0103
.200	2775.0 2770.7	9.84 11.87	05	.3899	.0779 .1108	.0324	.0010	.0005	0023 0031	.3975	.0101
.200	2775.7 2780.7	13.86 15.79	06 07	.3666	.1488	.0621	.0003	.0003	0021 0020	.5857	.0087
.200	2775.0	17.95	08	.7609	.2535	.0997	.000Z	0001	0009	.8020	.0067
.201 .200	2789.5 2772.7	19.23	08	.0409	.2924	.1126 0083	0012	0004	0020	.8716	.0058 .0105
			TEST 10			RUN .					
MACH	24	DEG	SETA DEG	CL	CD .	CMS	CPMS	CYMS	CYS	CN	CA
.200 .200	2778.1 2778.9	.01 -1.93	00 .01	.0626 .0402	.0113	0192 0251	0002	.0008 .0007	0014 0011	.0328	.0112
.200	2771.7	-4.34 .01	•02	0254	.0128	0346 0184	0003	.0009	0013 0016	0263	.0109
.201 .201	2786.7 2784.1	1.91	00 01	.1396	.0162	0153	0002	.0007	0017	.1401	.0116
.200	2773.7 2778.5	4.00 5.82	02 03	•2119 •2771	.0262 .0396	0083 0017	.0001	.0007	0013 0015	.2132 .2797	.0113
.200	2772.2	7.76 9.81	04	.3517 .4340	.0592	.0075 .0213	.0005	.0009	0017	.3565	.0111
.201	2794.5	11.78	05	.5196	-1190	.0360	.0010	.0009	0016	.5329	.0104
.200	2767.6 2781.0	13.91 15.78	06	.6137 .6978	.1620 .2065	.0536	.0010	.0006	0016 0014	.6347 .7277	.0097
.200	2764.5 2778.0	17.84 19.28	08 09	.7946 .8649	.2643 .3105	.0900 .1046	.0013	0001 0004	0008	.8374 .9190	.0082
.200	2780.4	.01	00	.0855	.0111	0193	0003	.0007	0015	.0855	.0111
			TEST 10	<b>.</b>	•	RUN ' 9					
HSAK	O.	ALPHA	SETA Deg	CL	. cs	ths	CHHS	CYMS	CYS 1	CH	CA
.200	2781.0	.01	00	.0903	.0147	0202	.0001	.0011	0010	.0903	.0147
.200 .200	2765.9 2774.6	-1.93 -4.51	.01	.0468 0214	.0131 .0161	0261 0356	0002 0001	.0010	0004 0014	.0463 0226	.0147 .0144
.201 .201	2782.8 2789.4	.06 1.92	00 01	.0930	.0146 .0198	0207 0168	.0064	.0011 .0011	0006 0007	.0930	.0145 .0149
.200	2777.6	3.86	02	.214A .2658	.0288	0109	.0015	.0009	0009	.2163	.0143
.200 .201	2767.7	5.85 7.77	03	.3595	.0638	0038 .0073	.0021	.0010	0004	.2888	.0143 .0146
.200 .200	2766.9 2764.3	9.82 11.92	05	.4439	.0919 .1293	.0201 .0341	.0023	.0008	0015 0011	.4531 .5553	.0149
.201 .201	2789.7 2788.7	13.90 15.78	06 07	.6338 .7239	.1720 .2195	.0486	.0025	.0004	0016	.6565 .7563	.0147 .0144
.200	2770.5	17.92	08	.8325	.2833	.0823	.0022	0000	0002	.8793	.0134
.200	2778.7 2779.8	19.22 •02	09	.8979 .0910	.3265 .0143	0204	.0019	.0010	0005 0001	.9553 .0910	.0127 .0142
			TEST 100	<b>.</b>		RUM 10					
MACH	•	ALPHA	BETA	CL	CO	CHS	CRMS	CYMS	CYS	CH	. CA
.200	PA 2774.4	.01	00	.1026	.0178	0237	.0001	.0008	0003	.1026	.0178
.201	2783.7	-1.90	.01	0002	.0160	0290	.0001	.0007	0010 0012	.0589 0015	.0179 .0178
.200	2757.9 2790.1	-4.20 .03	00	.1040	.0179	0373 0241	.0006	.0010	0006	.1040	.0179
•201 •200	2787.2 2776.1	1.91 3.89	01 02	.1546	.0232	0188	.0009	.0007	0010 0015	.1553	.0181
.200	2761.4 2774.3	5.82 7.80	03 04	.2894	.0486 .0710	0061 .0036	.0013	.0005	0021 0017	.2928	.0191 .0193
.200	2769.8	9.85	05	.4593	.0996	.0158	.0027	.0006	0011	.4696	.0195
.200	2772.7 2778.0	11.81	05	.5457	.1340 .1796	.0285 .0432	.0005	.0006	0015 0012	.5616	.0195 .0191
.199	2751.2 2775.6	15.82 17.94	07	.7371 .8414	.2287 .2920	.0590	.0004	.0003	0004	.7716 .8904	.0191
.201	2779.6 2772.1	19.51	09	.9194 .1047	.3452	0240	.0018	.6002	0021 0015	.9819	.0183 
		• 0 3	- 100		.01.4						

			HASA LANG			_					
			TEST 106	LEV		RUM 11	X 10 MIEN	SPEED TUR	MEL		
MACH	٩	ALPHA	BETA	CL	CD	CMS	CRHS	CYMS	CYS	CN	CA
NUMB -200	PA 2776.4	DE6 .01	DE6 00	.1190	.0208	0266	.0002	.0009	0010	.1150	.0207
.200	2761.8	-1.92	. 01	.0689	.0103	0319	.0002	.0008	0013	.0682	<b>.</b> 020 <b>6</b>
.201	2769.7 2779.2	-4.39 .01	00	.0054 .1150	.0205	0412 0268	000Z -0003	.0006	0012 0013	.0038 .1150	.0209 .0207
.201	2707.1 2774.5	1.69	01 02	.1676 .2340	.0267 .0379	0220 0157	.0007	.0007	0015 0013	.1684 .2361	.0211 .0221
.202	2805.5 2772.1	5.61 7.76	03 04	.3040	.0541	0087	.0012	.0009	0015	.3079	.0231
.201	2779.7	9.85	05	.4683	.1056	.0140	.0013		0013	.3061 .4795	.0235 .0239
.200	2769.2 2756.5	11.81 13.87	05		.1401	.0272	.0013	.0002	0012 0014	.5694 .6728	.0241 .0240
.201	2789.6	15.81 17.86	07	.7438	.2362 .2991	.0575	.0008	0002	.0003	.7800 .8994	.0246
.201	2781.4	19.21	09	.9209	.3469	.0874	.0016	.0000	0005	.9838	.0244 .0245
.200	2772.9	.02	00	.1156	.0205	0263	.0005	.0007	0011	.1156	.0205
			TEST 106			RUN 12		*			
MACH	•	ALPHA	BETA	CL	CD	. CMS	CRMS	CYMS	CYS	CH	CA
.200	0 PA 2765.1	DE6	00	.0919	.0144	0132	0001	.0009	0019	.0919	.0143
.200	2759.0	-1.92	•01	.0473	.0120	0206	0007	.0010	0012	.0491	.0136
.201	2782.2 2769.3	-4.21 .03	00	0168	.0129	0311 0133	0004	.0007	0016 0002	0177 .0923	.0117 .0144
.200	2767.3	1.94	01	.1479	.0205	0056	.0001	.0010	0012	.1485 .2080	.0154
.200	2767.8 2767.9	3.88 5.90	02 03	.2866	.0479	.0020	.0003	.0008	0004 0013	.2900	.0162 .0182
.201 .200	2778.4 2763.5	7.83 9.88	04 05	.3685 .4529	.0706 .1001	.0219 .0358	.0004	.0008	0015 0018	.3746 .4634	.0197 .0208
.201	2787.6	11.85	06	.5341	.1347 .1793	.0515	.0005	.0008	0016	.5503 .6498	.0221
.201 .201	2780.1 2780.8	13.92 15.85	07	.6250 .7130	.2284	.0866	.0011	0002	0008	.7482	.0236
.200 .201	2755.4 2786.1	18.03 19.27	08	.8135 .8722	.2928 .3341	.1064 .1215	.0014	0000	0025	.8641 .9336	.0265 .0276
. 500	2773.9	.04	00	.0915	.0145	0129	0004	.0009	0008	.0915	.0144
			TEST 106								
	_					RUN 13	****				
MACH Numb	PA	ALPHA Deg	BETA Deg	CL	CD	CHS	CRMS	CYMS.			CA
.200 .201	2772.9 2778.9	.08 -1.91	00 .01	.0866	.0266	.0132 0039	0002 0004	.0009	0022	.0867	.0264
.200	2759.9	-4.22	.02	0424	.0242	0185	0004	-0004	0028	0441	.0210
.200	2765.1 2776.7	.07 2.01	.00 01	.0880	.0267 .0347	.0122 .0176	0008	.0006	0035 0034	.0860 .1423	.0266
.200 .200	2761.1 2776.0	3.92 5.91	02	.2017 .2733	.0468	.0255	0002	.0004	0041 0046	.2044 .2785	.0329
.200	2759.2	7.86	04	.3689	.0926	.0438	0002	.0004	0044	.3781	.0413
.200 .200	2776.3 2757.7	9.92 11.99	05	.4614	.1266	.0560 .0732	.001Z	.000Z 0007	0046	.4763 .5727	.0452
.200	2758.4 2766.1	13.95	06 07	.6326	.2111	.0907	.0020	0014 0015	0053	.6649	.0523
.201	2784.1	17.99	08	.8126	.3272	.1287	.0019	0015	C057	.8739	.0602
.200	2775.8 2754.9	19.38	08	.8789 .0862	.3759 .0273	.1430 .0126	0003	0021 .0004	0057 0051	.9539	.0630 .0272
			TEST 106			RUN 14					•
MACH	٥	ALPHA	BETA	CL	CD	CHS.	CRHS	CYMS	CYS	CN	CA
.201	0 PA 2779.2	DEG . 12	DEG	.0971	.0458	.0264	.0002	.0004	0034	.0972	.0456
.200	2760.7	-1.87	.01 .02	.0175 0470	.0395	.0093 0061	0000	.0006	0029	-0162	.0400
.200	2755.8 2767.4	-4.11 .10	•00	.0959	.0453	.0262	0002	.0003	0033	.0960	.0452
.200	2765.5 2754.3	2.03 4.00	01 02	•1507. •2208	.0565 .0719	.0413	.0001	.0002	0032 0039	.1526 .2252	.0511
.201	2781.4	5.94	03	. 2860	.0905	.0579	.0064	2000	0041	.2935	.0605
.200	2765.2 2767.1	7.92 9.98	03 04	.4450	.1148	.0751	.0014	0013	0059	.3668	.0704
.200	2770.6 2773.7	11.92 13.98	05 06	.5314	.1901 .2375	.0082	.0013	0017 0017	0058 0055	.5592	.0762
.Z00	2768.4	15.90	07 07	.7005	.2898	.1192	.0018	0021	0063	.7530 .8554	.0868
.201	2783.8 2780.4	17.97 19.61	08	.7853 .8464	.4038	-1524	.0021	0030	0059	.9328	.0963
. 200	2762.3	.12	.00	.0982	.0463	.0261	.0004	.0004	0033	.0983	.0461
			TEST 106			RUN 15		•			
MACH NUMB	g PA	ALPHA Deg	BETA DEG	CL	CD	CHS	CRMS	CYMS	cáz	CH	CA
.200	2763.6 2759.6	-1.85	.00 .01	.0994 .0397	.0579 .0527	.0278 .0151	.0011	.0006 8000.	0048	.0999	.0576
.199	2743.8	-4.15	•02	0250	.0515	.0008	.0010	.0009	0039	0286	.0495
.201 .200	2782.2 2774.1	.15 2.07	.00 01	.1057 .1749	.0560	.0279 .0388	.0012	.0007	0053 0051	•1056 •1772	.0577 .0617
.201	2781.0 · 2768.2	4.00	02	.2369	.0836	.0486	.0005	.0002	0040	.2422 .3072	.0669
.201	2776.8	7.94	03	. 3650	.1293	.0661	.0007	0016	0033	.3794	.0777
.200	2774.4 2781.8	9.97 11.99	04	.4422	.1636	.0777 .0896	.0007	C009 0014	0039	.4639	.0845 .0911
.201 .201	2785.4 2796.1	13.9A 15.94	06	.6043	.2518 .3038	.1030 .1176	.0008	0014 0019	0052	.6472	.0983
. 201	2777.0	17.94	07	.7687	.3647	.1338	.0013	0025	0076	.8437	.1102
.201	2792.5 2776.3	19.54	08	.0326	.4175 .0581	.1468 .0250	.0016	0032	0080 0057	.9243 1143	.1150

		MASA LANGLEY				. 7	X 10 HICH	SPEED TUN	NEL .		•
			TEST 10	•		RUM 16					
MACH	9	ALPHA	BETA	CL	CD	CHS	CRMS	CYMS	CYS	CH	CA
NUMB • 201	PA 2791.7	0EG .12	DEG .00	.1126	20502	.0255	0012	0005	0036	.1127	.0579
.200	2774.3	-1.83	.01	.0491	.0526	.0124	0010	0004	0036 4	.0474	0541
. 200	2773.7	-4.18	-02	0175	.0510	0026	0017	0006	0032	0212	.0496
.201	2784.6 2784.9	.13 2.04	.00 01	.1153	.0579 .0679	.0247	0007	0006	0049	.1154 .1058	.0576 .0614
.200	2773.3	4.07	02	.2450	.0846	.0474	.0000	0008	0064	.2504	.0670
.200	2782.9	5.95	02	.3031	-1041	.0556	.0004	0009	0064	.3122	.0721 .0777
.201 .201	2786.2 2785.2	7.92 10.01	03 04	.3686	.1297 .1651	.0773	•0004	0012	0049	.4703	.0847
.200	2770.9	11.91	05	.5233	.2032	.0886	.0006	0020	0069	.5539	.0908
.200 .202	2760.8 2021.7	13.97 15.90	06 06	.6063	.2521	.1024	.0008	0022	0073 0082	.6512 .7422	.0976 -1036
.202	2794.9	17.94	07	.7720	.3664	.1332	.0009	0028	0091	.8473	.1108
.201	2805.1	19.46	08	. 6261	.4143	.1452	.0011	0034	0087	.9188	.1148
•200	2703.4	.14	•00	.1169	.0578	.0237	0004	0006	0096	.1191	.0576
			TEST 10	6		RUN 17					
MACH	۵	ALPHA	RETA	CL	CB	CMS	CRMS	CYMS	CYS	CH	CA
NUMB	• 4	DEG	BETA DEG .00 .01 .02 .00 -01 -02 -03								-
.201	2794.9	.12	.00	.1257	.0451	.0177	.0013	.0004	0028	-1258	.0448
.200	2776.9 2782.6	-1.96 -4.10	.01	.0461 0213	.0381	.0013 0165	0002	.0005	0025 0023	.0447 0238	.0396
.201	2003.0	.11		.1257	.0455	. 21 + 5	.0020	.6603	0030	.125#	.0452
.201	2786.3	2.03	01	.1781	.0571	.0340	.0003	.0007	0033	.1860	.0507
.200	.2771.2 2770.9	4.01 5.92	02	.2390 .2933	.0724	.0457	.0008	0015	.0013 0016	.2435 .3011	.0595
. 200	2779.4	1.77	03	.3607	.1156	.0655	.0010	0003	0040	.3733	.0643
-201	2785.4	9.94	04	4472	.1492	.0753	.0013	0010	0039	.4662	.0698
.200	2777.9 2775.2	11.96 13.96	05 06	.5352 .6178	.1905	.0878	.0015	0015 0019	0055	•5630 •6566	.0754
.Z00	2774.3	15.96	07	.7059	.2918	.1201	.0018	0016	0059	.7590	.0865
.200 .201	2774.7 2804.9	16.01 19.54	07 08	.7877 .8501	.3525	.1369	.0023 .0021	0025 0024	0061 0053	.8561 .9361	.0916
.201	2788.3	.12	00	.1297	.0462	.0183	.0017	.0006	0019	.1298	.0459
			TEST 10	6		RUN 18					
	_							•			
MACH NUMB	PA	ALPHA Deg	8ETA DEG 00 -01 -02 00 01 02 03	CL	CD	CMS	CRMS	CYMS	CYS	CH	CA
.200	2780.1	.06	00	.1234	.0316	0001	.0001	.0006	0018	.1235	.0317
. 200	2776.1	-1.86	.01	.0547	.0273	0137	.0004	+0005	0018	.0538	.0291
.200 .201	2772.3 2784.1	-4.09 .09	- 02	00A8 .1262	.0267 .0324	0252	0004 0001	.0000	0025 0022	0107 .1263	.0260
.200	2759.0	2.00	01	.1720	.0409	.0084	.0004	.0004	0026	.1742	.0348
.200	2776.3	3.94	02	.2284	.0528	.0160	.0005	.0002	0033	.2315	.0370
•200 •200	2772.5 2766.6	5.90 7.88	03	.3083	.0730 .1065	.0235	.0005 0014	.0001 0001	0021	•3142 • •4292	.0409
-200	2774.3	9.93	04	.5042	.1409	.0439	0007	0003	0037	.5210	.0518
.200	2769.4	11.91	֥05	.5693	.1812	.0592	0002	0005	0024	-0141	.0557
.200 .200	2775.3 2764.7	14.03 15.91	06	.6777 .7645	.2307 .2840	.0780 .0952	.0007	0011 0004	0038	.7134 .8131	.0595
.199	2741.9	17.96	05	.8592	.3496	.1141	.0020	0011	0056	.9251	.0676
•200 •200	2763.9 2760.5	19.65	08 .00	.9408	.4119	.1313	.0003	0019	0055 0026	1.0245	.0716
*****	2700.7		•00		.0327		******		-10020		.0363
			TEST 10			RUN 19					
			163. 10								
MUMB	ý PA	AL PHA DEG	BETA	-CL	60	CKS	CRMS	CYMS	CYT	CN.	. CA
.201	2781.4	.12	•00	.1365	.0525	.0152	.0020	0000	0026	.1366	.0522
.200	2772.5	-1.95	.01	.0541	.0446	0014	.0004	.0003	0020	.0526	.0464
.2G0 .201	2777.5 2787.9	-4.22 .09	.00	0121 .1352	.0430	0153 .0152	.0005	0001	0022	0152 -1353	.0420
.201	2784.4	2.01	01	.1692	.0641	.0303	.0003	.0000	0031	-1914	.0574
.200	2766.2	4.06	TEST 10  BETA DEG .00 .01 .02 .00010202020304	. 2624	.0818	.0395	.0003	0003	0029	.2675	.0630
.200	2776.4	5.92 7.90	02	.3248	.1016	.0465	.0004 .0002	0016 0016	0015 0032	.3335 .4187	.0675
.200	2772.2	9.96	04	4994	.1683	.0617	.0001	0015	0039	.5209	.0794
.200	2779.4	11.97	05	.5884	.2125	.0747	.0009	0016	0032	-6197	.0859
-200 -201	2772.0 2780.0	13.98 15.90	06	.6716 .7524	.2616 .3152	.0889 .1058	.0014 .0011	0021 0015	0046	.7151 .8100	.0915
.200	2773.6	17.95	07	.8317	.3769	.1236	.0021	0028	0061	.9073	.1022
.201	2796.8	19.41	08	.8927	.4277	.1374	.0024	0034	0054	.9841	.1066
.201	2790.6	.11	•00	.1407	.0526	.0156	.0016	0002	0026	.1408	.0524
			TEST 10			RUN 20					
MACH	, O , P.A	ALPHA Deg	BETA	CL	CO	CMS	CRHS	CYMS	CAZ	CH	Ca
.200	2781.5	.13	.00	.1278	.0634	.0214	.0001	0004	0042	.1280	.0631
.201	2785.1	-1.83	.01	.0623	.0573	.0091	.0003	0003	0041	.0605	.0593
.200	2769.3 2776.4	-4.13 .14	.02 .00	0047 .1306	.0551	0042 .0216	.000	0005	0038	0087 -1307	.0546
. Z00	2780.4	2.13	01	.1984	.0756	.0335	0000	0004	0043	.2011	.0682
.201	.2785.6 '2782.5	4.03	02	.2573	.0924	.0436	.0003	0007	0049 0035	.2632	.0741
.200 .200	2782.5	5.95 7.91	02 03	.3205 .3974	.1136 .1432	.0500	.0002 0002	0026	0040	.3306 .4133	.0778
.200	2770.7	10.06	04	.4789	.1819	.0695	0007	0016	0056	.5034	.0952
.200	2767.9	11.92	05	.5543	.2210	.0811	0004	0019 0021	0069 0078	.5880 .6893	.1018
.200	2780.3 2774.3	14.05	06 07	.6421 .7224	.3268	.1062	0006	0019	0087	.7843	.1165
. 200	2767.3	18.11	07	.8148	.3967	.1226	0004	0026	0090	.8977	.1230
.201	2786.6 2788.3	19.38	08	.8626	.4382	.1319	.0003 0001	0037 0006	00#8	.9591 .1321	.1271
		•••	•••						<del>-</del>		

TABLE II. continued

			MASA LANG	SLEY -	7 % 10 MIGH SPEED TUNNEL				MEL		
			TEST - 10	<b>.</b>		RUN 21					
HACH	0 PA	ALPHA Deg	BETA DEG	CL	CD	CHS	CRHS	CYMS	CYS	CH	` CA
.200	2780.3 2764.8	.03 -1.99	00 .	.1055	.0208 .0178	0156 0236	.0005	.0005 .0007	0012 0006	.1055	.0207 .0196
.200	2780.9	-4.36	.02			0343	.0004	.0005	0009	0070	.0108
.201	2797.6	.06 1.92	00 01	.1576	.0271	0164	.0004	.0003	C012 0016	.1047 .1564	.0203
.200	2777.8 2783.8	3.89 5.84	02 03	0056 .1046 .1576 .2231 .3033 .3866 .4747 .5681 .6668 .7593	.0385	0018	.0010	.0004	0007 .0002	.2252	.0232 .0265
.200	2767.3	7.81	04	.3866	.0826	.0176	0003 0011	.0005	0010	.3076	.0293
.200	2784.6 2770.2	11.86	05 06	.5681	.1533	.0312 .0442	0011	.0008	0012	.4873 .5874	.0311
.201	2785.5 2772.4	13.93 15.86	06 07	.6668 .7593	.2021 .2548	.0590	0010	.0003	0008	.6958	.0356 .0375
.200	2782.5	17.91	~.08	.8634	.3207	.0943	0005	.0009	0020	.9207	.0395
.200	2776.8 2776.7	.03	00	.9356 .1062	.3730 .0207	.1095 0162	.0002	.0002		1.0064	.0410
			TEST 100	•		RUN 22.					
HACH	PA	ALPHA	BETA	CL	CD	CAS	CRHS	CYMS	CYS	4.54	CA
.200	210101	DEG .03	0EG	.0648	.0118	0056	0004	.0009	0006	.0648	.0117 .0107
• 200 • 200	2781.8 2767.4	-2.05 -4.15	.01 .02	.0160 0410	.0101 .0125	0150 0226	0003	.0010	0007 0009	.0156 0419	.0107 .0095
.201	2785.1	. 33	00	.0655	.0116	0057 .0019	0003	.0009		.0555	.0116
.201	2791.9 2775.0	.03 1.93 3.89 5.91	01	.1794	.0259	.0095	0002	.0008	0011	.1214 .1807	.0125 .0136
.200	2775.6 2764.2	5.91 7.80	03 04	.2540	.0417 .0634	.0196	.0009	.0006	0009	.2570 .3416 .4326	.0153 .0172
.201	2790.3	7.80 9.93 11.87	05	-0160 -0410 -0655 -1209 -1794 -2540 -3361 -4230 -5013 -5881 -6757	.0927	.0458	.0009	.0009	0009 0012 0009 0011	.4326 .5164	.0184
.200	2763.5 2780.2	13.90	06 06	5841	.1668	.0607	.0010	.0008	.0014	.6109	.0206
.200	2758.8 2772.9	15.86 17.88	07 08	.6757 .7686	.2147 .2723	.0963	.0017 .0016	0005	0009 0001	.7087 .8151	.0219 .0232
.201	2794.4	19.35	09 00		.3205	.1318 0041	0009	0001 .0007	0013 0001	.8979	.0243
• 201	2140.0	•03		*	10110			***************************************	0001	.0037	
			TEST 100	.0661 0070 0055 .0681 .1242 .1803 .2528		RUN 23					
MACH	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	ALPHA	BETA Deg	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
. 200	213001	0 E G	00	.0661	.0216	.0155	0007	.0011	0011	.0661 0077	.0235
.200	2763.3	-1.90 -4.13	00 .01 .02 00 01 02 03 04 04 05	0655	.0210	.0016 0119	0011	.0004	0014	0670	.0207 .0164
.200	2768.9 2762.3	2.03	00	.0681	.0236 .0308 .0413 .0578	.0155	0011	.0007 .0007	0017 0019	0670 .0681 .1252 .1829 .2574	.0235
.200	2769.2	3.99	02	1003	.0413	.0309	0005	.0007	0020	.1029	.0287
•201 •201	2772.3 2779.6	5.88 7.86	03	.3385	.0578	.0399	.0002	.0006	004Z	.3465	.0351
.200	2761.1 2768.0	9.91	04	.4285 .5082	-1160	.0635	.0008	0006	0035	.4410	.0385
.201 .200	2771.0	13.94	06 07	.5950	.1945	.0984	.0010	0010 0013	0033	.6243 .7193	.0454
.200	2763.5 2750.7	17.93	08	.7725	.3052	.1360	.0024	0012	0050	.8289	.0526
.200	2766.4 2763.4	.12	06	.8536 .0731	.3642	.1541	.0025 0018	0016	0045 0021	.9263 .0731	.0561
			TEST 106	•		RUN 24					
MACH	FA	ALPHA	BEFA	CL	CP.	CMS	CRMS .	C~45	C+\$	CH	T4
NUMB . 201	2771.2	DEG .12	DEG .00 .01 .02 .00 01	.0898	.0424	.0286	0008	0002	0024	.0899	.0422
.200 .200	2756.9 2768.3	-1.93 -4.13	.01	.0099 0545	.0366	.0119 0043	0016 0017	0001 0002	0015 0016	.0086 0570	.0371 .0326
.201	2771.2 2781.0	.11	.00	.0898 .0099 0545 .0901 .1423	.0425	.0290	0003 0010	0002	0017 0020	.0902	.0423
• 201 • 200	2767.0	3.95	02	.2093	.0666	.0530	0003	.0004	0032	.2134	.0521
.201 .201	2776.7 2776.4	5.88 7.85	03 03	.2625	.0831 .1058	.0623 .0717	.0002	0001 C024	0034 0013	.2697 .3382	.0557 .0601
.200	2765.9	9.92	04 05	.4144	•1391 •1771	.0828	.0011	0015	0043	.4322 .5238	.0656
.200	2759.1	13.92	06	.5834	.2231	.1113	.0014	0021	0044	.6200	.0762
.201 .201	2771.6 2775.9	15.86 17.92	07 07	.6641 .7490	.2731 .3337	.1276 .1469	.0018	0024	0055 0061	.7134 .0154	.0812 .0870
. 201	2780.5 2774.5	19.36	08	.8083	.3001 .0423	.1602 .0276	.0015 0011	0025 0002	0053 0021	.8887	.0906 .0422
			TEST 100	•		RUN 25					
MACH	•		BETA	CL	CD	C#3	CRMS	LYAS	C/S	CH	- CA
NUMB .201	PA 2777.1	.12	0E6 .00	.0859	.0545	.0327	0007	0002			.0543
.200	2768.0 2770.1	-1.06 -4.10	•01	.0240 0357	.0503	.0199	0004	0000	0031	.0860	.0511
.200	2765.2	.11	.00	.0854	.0545	.0067	0009	0001	0027	0392	.C472
.201	2775.8 2762.2	2.02 4.03	01 02	.1529	.0636	.0448	0003	.0000	0035	.1551 .2144	.0581 .0630
.201 .201	2774.4 2776.0	5.92 7.89	02	.2686	.0961	.0638	.0006	0008 0010	0029	.2771 .3497	.0679
.201	2778.1	9.95	04	.4089	.1525	.0847	.0007	0009	0031	.4291	.0732
.200	2753.8 2768.2	11.90 13.97	05 06	.4842	.1894	.0962	.0009 .0012	0010 0020	0038	.5128	.0055
.201 .201	2791.3 2788.2	15.88	07 07	.6461 .7301	.2055 .3461	.1238	.0011	0021	0057	.6996 S108.	.0977 .1044
.201	2782.9	19.55	08	.7945	.3978	.1540	.0018	0029	0064	.8818	.1090
.200	2767.3	.15	.00	.0883	.0549	.0325	0003	.0000	0032	.0884	.0547

TABLE II. continued

		MASA LAN	GLEY		1	X 10 HIGH	SPEED TUN	NEL			
			TEST 10	•		RUN 26					
MACH		ALPHA	BETA DEG .00 .01 .02 .00 01 02 03 04 05 07	CL	CD	CHS	CRMS	CYMS	CYS	CN	CA
MUMB .201	7A7.0	0 E G	DEG	.1356 -0060 -0009 -1366 .2032 .2649 .3279 .3968 .4792 .5512 .6369 .7197 .8005	.0604	.0204	.0001	.0001	0036	.1359	.0601
.200	270201	-1.83 -4.30	.01	.0660	.0541	.0074	.0003				.0562
.200	2742.Z 2760.6	-4.30 .14	•0Z	0035	.0525	0064	.0003	.0001	0036	.1367	.0600
.201 .200	2778.0	2.06	01	.2032	.0713	.0314	0001	0003	0036	.2056 .2700	.0639
.201	2742.2 2760.6 2778.0 2753.8 2774.1 2773.2 2766.6 2773.1 2790.6	5.95	02	.3275	.1092	5040	- 0006	0008	0038 0036 0036 0043 0043 0029	.3370	.0747
.201 .200	2773.2 2766.6	7.97 9.97	03 04	.3968 .4752	•1374 •1732	.0591	.0007	0012	0029	.4120 .4980	.0810
.201	2773.1	11.94	05	.5512	.2130	.0817	.0011	0013	0052	.5836	.1021
.200	2/00.7	15.90	07	.7157	.3172	.1100	.0014	0015	0071	.7752	.1089
.200 .201	6/7607	17.00 19.35	07	.8005	.3815 .4258	.1266	.0018	0027	0069 0070	.8792 .9440	.1157 .1198
.201	2783.6 2780.1	-16	.00	.8510	.0605	.0202	.0002	0001	0048	.1353	\$000
				٠							
		•	TEST 100	<b>)</b>		RUM 27					
MACH	Q PA 2760.7 2761.3 2743.0 2768.0 2761.5 2758.3 2758.4	ALPHA	\$ETA 0E6 .00 .01 .02 .00 01 02 02 03 04 05 06 07 07	CL	CO	CMS	CRMS	CYMS			
.200	2760.7	.12	.00	.1369	.0492	.0179	.0022	.0001	0035	.1370	.0489
.200	2761.3 2763.0	-1.94 -4.32	.01	.0549	.0413	.0003 0171	.0000	.0006	0027	.1370 .0535 0224	.0431
.201	2768.0	•11	.00	.1361	.0492	.0182			0044	**301	
.200	2761.5 2758.3	2.02 4.01	01	.1869	.0609 .0770	.0325	.0008	.000Z	0031	.1889 .2640	.0543
. Z90	2758.4	5.92	02	.3149	.0957	.0412 .0499 .0577	.0009	0021 0027	0024	.3231	.0627 .0679
.200	2765.7	7.89 9.95	04	.4798	.1596	.0673	.0012	0018	0045	.5001	.0743
.201	2773.1 2758.2	11.91	05	.5651	.2008	.0792	.0012	0023	0056 0061	.5944 .6923	.0798
. 200	2751.8	15.94	07	.7290	.3031	.1126	.0016	0020	0080	.7842 .8857	.0912
.201	2770.0 2789.1 2773.0	17.95 19.38	07	.5126 .5687	.4126	.1313	.0020	0026 0037	0069 0076	.9564 .1377	.097Z
.201	2773.0	•11	•00	.1377	.0492	.0177	.0018	0000	0042	.1377	.0490
			TEST 104			8UN 28					
			8ETA DEG00 .01 .0200 .01 .0201 .0203040405060708	•		RUM 20		•			
MACH	PÅ	ALPHA Deg	BETA	CL	CD	CMS				CN	
.201	2774.7	.06	00	.1222	.0288	.0024 0124	0005	.0010	0009	.1222 .0451 0125 .1195 .1727	.0287
.200	2759.4	-4.15	.02	0108	.0239	0253	.0005	.0008	0009	0125	.0231
.200	2759.6	•07 1•97	00 01	.1194	.0286	.0020	0004	.0010	0005 0019	.1195 .1727	.0285
.200	27¢2.6	3.99	02	.2340	.0500	.0176		.0000	002	.2304	.0336
.200	2757.2 2749.9	5.93 7.88	03	.4041	.0708	.0256 .0342		.0005	0008 0027		.0377 .6417
.201 .201	2770.9	9.93	04	.4936	.1324	.0483	.0013	0013	.0006	.5090 .5950	.0453
.200	2757.7	13.99	06	.6579	.2184	.0634	.0012	0009	0017	.6911	.0529
.200 .200	2739.6 2740.9	15.99 17.94	07	.7477 .8362	.2734 .3357	.1022 .1210	.0015	0002	0032 0030	.6911 .7941 .9009	.0569
.201	2772.8	19.57	06	.9149 .121f	.3940	.1371	0024	0014 .00J1	0032	.9940	.0648
.200	2751.3	. 07	00	.1211	.0186	.0323	-10003	10071	.0002		·vepi
			TEST 10	·	•	RUM 29					
MACH	٩	ALPHA	BETA	CL	co	CHS	CRMS	CYMS	CYS	CH	CA
.200	PA 2753.8 2744.6 2741.9 2761.9	DE6	BETA DEG 00 .01 .02 00 01 02 03	.0984	-0176	0154 0229 0324 0151 0078 0006	. COO6	.0011	0008	.0984	.0176
.200	2744.6	-1.93	.01	.0538	.0151	0229	0003	.0008	0008 0017 0014	.0333	.0169
.200	2741.9 2761.9	-4.26 .03	02 00	0108 .0997	.0162	0324	.0005	.0008	0013	0120 .0997	.0174
.201	2771.5 2750.9	1.93 3.98	01	.1543	.0239	0078	.0011	.0010 .0009	0012 0017	.1550	.0187 .0196
.200	2759.6	5.85	03	3031	.0531	.0057	.0014	.0009	0015	.3070	.0219
.201 .201	2776.4 2762.6	7.84 9.99	04	.3862 .4760	.0773 .1098	.0326	.0019	.0009	0015 0016	.3931	.0239
.200	2759.2	11.69	05	.5576	.1449	.0458	.0013	.0007	0007	.5755	.0269
.200	2757.2 2752.4	13.92 15.87	06 07	.6483 .7383	.1901 .2413	.0621 .0801	.0019	0001 0008	0009	.6750 .7761	.0285
. 201	2775.6 2748.2	17.92	08	.8305	.3017 .3566	.0995	.0020	0003	0028	.8830 .9739	.0316
.200	2739.0	•06	00	.1032	.0177	0136	.0006	.0011	0011	.1032	.0176
	•							•			
			TEST 100	•		RUN 30		_			
MACH	PA	ALPHA Deg	BETA Deg	CL	CD	CMS	CRHS	CYMS	CYS	CN -	CA .
.201	2804.0	• 02	00	.0074	.0083	.0060	0007	.0008	0010	.0074	.0003
.200 .200	2778.0 2772.3	-1.46 -4.35	.01	0433 1141	.0094 .0158	0006	0007 0011	.0008	0010 0013	0436 1150	.0079
.200	2777.3 2793.3	.03 1.91	00	.0059	.0084	.0055	0007 0004	.0005	0008	.0059	.0084
.200	2768.1	3.93	02	.1163	.0170	.0117 .0201	0004	.0005	0012	.1172	.0090
.200	2780.7 2781.3	5.81 7.79	03 04	.1818	.0279 .0444	.0301	0002 2000.	.0004	0007 0010	.1837	.0094
.201	2793.0	9.86	05	. 3356	.0682	.0561	.0005	.0003	0023	.3423	.0098
.200 .199	2782.1 2754.5	11.61 13.92	05	.4160	.0972 .1353	.0715	.0005	.0004	0017 0021	.4271 .5216	.0100 .0102
.201	2801.3	15.81 17.87	07 08	.5861	.1772 .2316	.1064 .1269	.0011	0001 0008	0017	.6142 .7228	.0103
.202	2820.0	19.40	08	.7540	.2764	.1426	.0013	0011	0006	.8030	.0103
. 201	2785.3	.03	00	.0093	.0086	.0068	0005	.0004	0011	.0093	.0086

	MASA LAMELEY					7 % 10 HIGH SPEED TUNNEL					
			TEST 104			RUN 31					
MACH		ALPHA	BETA	cı	CD	CHS	CRMS	CYMS	CYS	CN	CA
.200	0 PA 2775.1	. 05	DE6 00	.0152	.0143	.0182	0010	.0011	0004	.0152	.0143
.200		-1.42	•01	0458	.0138	0045	0007	.0011 .0010 .0005	0006	0463 (	.0123 .0104
.200	2778.1	.05		.0159	.0142	.0186	0011	.0012	00G6 0014	.0159	.0142
.201	2792.3	3.92	02	.1211	.0180	.0352	0004		0006	.0642 .1226	.0156 .0175
.200	2765.0 2789.2	5.87 7.82	03	.1050	.0385	.0453	0001	.0004	0014	.1879 .2698	.0193 .0218
.200	2760.7	9.87	05	.3477	.0848	.0721	.0004 .0004	.0009	0007 0014	.3571 .4428	.0240
.201	2790.9	13.99	06	.5183	.1584	.1079	- 0010	. 0000	0024	.5412	.0283
.200	2775.0	17.92	07 08	•600 <b>9</b> •6926	.2024	.1256 .1461	.0014	0006	0022	.6333 .7387	.0306
.201	2768.6 2778.1 2788.9 2792.3 2765.0 2769.2 2760.7 2753.0 2790.9 2775.0 2804.0 2795.7 2784.9	19.35	09	.1050 .2644 .3477 .4280 .5183 .6009 .6526 .7596	.3043	.1615 .0189	.0015 0010	0005 -0011	0022	.8176 .0171	.0351 .0143
			TEST 106			RUN 32					
MACH	۵	AI BUA	BETA	CL	CD	CHS	CRHS	CYMS	CYS	CM	CA
NUMB	PA 2786.0 2782.5 2770.1 2803.5 2765.8	DEG	DEG								
.201	2786.0 2782.5	-1.91	00 .01	.0751 .0077 0457 .0665 .1239 .1817	.0173	.0017 0086	0009	4000. 5000	0012	.0751 .0072	.0172 .0156
.200	2770.1	-3.65	•02	0457	.0175	0178	0014 0017	0008	0008 0011	0467	.0144 .0179
.201	2785.8	1.95	01	.1239	.0237	.0093	0005	.000	0018	.1246	.0195
.201 .201	2788.8 2795.0 2786.8	· 3.91	02	•1817 •2452	.0337	.0183 .0296	0004		0024 0027	.1836 .2489	.0212 .0233
.201			04	.3307	.0721	.0390			0025 0018	.3374 .4182	.0264 .0292
.200	2772.1	11.87	05	4951	.1359	.0709	.0010	0004	0030	.5125	.0311
.200	2778.1 2758.0	13.94	06 07	.5817 .6641	.2769	.0893 .1079	.0008	0010 0016	0034 0034	.6077 .7006	.0335
.200	2772.1 2776.1 2758.0 2781.4 2785.4	17.94	05	.7586	.2866	.1285 .1461	.0010	0011 0014	0041 0037	.8100 .8977	.0359
.200	2781.2	.00		.1817 .2452 .3307 .4669 .4951 .5817 .6641 .7586 .8322	.0183	.0027	0016	0002	0009	.0665	.0183
		•	TEST 106	!		RUN 33		,		•	
MACH	0 PA	ALPHA	8ETA OFG 00 .01 .02 00 01 02 03 04 04 05 06	CT.		CHS	CRMS	CYMS		CH	CA
.200		.05	00	.0847 .0226 0401 .0880 .1337 .1910 .2707 .3671 .4414 .5244 .6088	.0196	0015	0006	.0005 .0004 .0002 .0006	0006	.0847	.0196
.200	6/0347	-1.94 -4.28	.01	.0226 0401	•0167 •0169	0116 0235	-0000	+0004 -0002	0002	.0221 0414	.0175 .0159
-201	2807.2	.04	00	0880	.0200	0029	0005	.0006	0009	.0880	.0199
.201	2795.3	3.89	02	.1910	.0369	.0056 .0149	0014 0013	.0002	0016	.1345 .1930	.0222
.200	2775.9 2787.0	5.85 7.83	03	.2707	.0541	.0235 .0306	0007		0014	.2748 .3745	.0263
.Z00	2778.5	9.89	04	. 4414	.1099	.0471	.0000	0000	0018	.4537	.0325
.200	2784.2	13.93	05	.6068	.1093	.0637	.0015	0003	0032	.5431	.0346
•201 •200	2763.2 2807.2 2800.9 2795.3 2775.9 2787.0 2776.8 2784.2 2809.2 2709.8 2805.2	17.92	07	.6924 .7842	.2379 .2982	.1011	.0000	0011 0003	0005 0017	.7311 .8379	.0396 .0424
.201	2805.2 2786.0	19.50	09	.8560 .0720	.3507 .0212	.1387 .0030	0031	0007 0002	0015	.9240	.0445
			TEST 106			RUN 34	•				
MACH	. 0	ALPHA	SEIA	- CL	~ cu	EMS	CRHS	CYMS	CYS		C.A
NUM8	74 2770.4 2775.6 2793.0 2786.8	DEG	DEG 00 01 02 03 03 04	.0656	-0115		0006		0010	-	.0115
.200	2775.0	-1.94	.01	0004	.0114	0124	0003	.0005	0009	0008	.0114
.200	2783.0 2786.8	-4.20 .05 1.92	00	0654	.0158	0196 0050	.0000	.0004	0017 0027	0664	.0110
.201	2792.2 2782.0	1.92 3.90	01	0897	.0159	.0026	0007	.0001	0028 0029	.0902 .1640	.0129 .0132
.200	2779.7	5.85	03	.2314	.0371	.0177	•0022	.0005	0034	.2339	.0134
.200	2702.9 2773.1	7.60 9.95	03	.3027	.0558	.0292 .0436	.0031	.0004	0046	.3075	.0141 .0147
.200	2771.6 2779.3	11.83 13.98	05 06	.4724 .5673	.1144	.0569	.0033 .0037	.0003	0045 0047	.4859 .5885	.0151 .0156
.200	2773.8	15.82	07	.6540	.2019	.0907	.0035	COOB	0031	.6843	.0160
.201	2864.4 2768.8	17.90 19.17	08	.7537 .8127	.2606 .2999	.1097	.0032	0013 0007	0033 0040	.7974 .8661	.0163
200	2775.4	.05	. •00	.0335	0126	0029	.0010	.0006	0050	.0336	.0126
			TEST 106			RUN 35					
MACH NUMB	PA	ALPHA DFG	BETA DEG	, cr	CD	CM2	CRMS	CYMS	. (12	Ch	C÷
.200	2760.4 2781.5	.03 -1.91	-4.99	.0112 0463	.0190 .0176	.0209 5800.	.0039	C076 0082	.0199 .0208	.0112 0468	.0190
.200	2777.3	-4.18	-4.96	1098	.0202	0047	0001	0086	.0227	1110	.0121
.200	2784.0 2780.9	.06 1.95	-4.99 -5.00	.0115	.0191 .0240	.0211 .0337	.0039 .0052	0080 0073	.0194 .0156	.0115 .0663	.0190 .0218
.201 .200	2786.3 2767.4	3.92 5.91	-5.00 -4.99	.1234	.0332	.0441	.0062 .0114	0086	.0130	.1253 .1906	.0247 .0280
.200	2779.5	7.87	-4.97	. 2532	.0667	.0698	.0121	0122	.0079	.2599	.0314
.200	2782.8 2773.9	10.00	-4.95 -4.92	.3437 .4187	.0967 .1285	.0852	.0147 .0167	0173 0211	.0110	.3553 .4362	.0355
.200	2776.1 2793.8	14.00 15.92	-4.88 -4.85	.5071 .5875	.1710 .2160	.1168	.0186 .0205	0233 0245	.0120 .0064	.5334	.0432
.201	2789.1	16.12	-4.80 -4.77	.6810 .7364	.2766 .3165	•1572 •1702	.0218	0269	.0006	.7332 .7997	.0511
.200	2782.7 2783.2	19.43	-4.99	.0096	.0199	.0214	.0035	0083	.0187	.0096	.0199

TABLE II. continued

MASA LANGLEY						7	X 10 HIGH	SPEED TUN	HEL		==
			TEST 10	6		RUM 36					
HACH		ALPHA	BETA	CL	CD	CMS	CRMS	CYMS	CYS	CH	CA
NUM 8	2774.0	DFG 02	-4.99	0029	.0063	.0008	.0027	0075	.0266	0029	.0063
.200	2766.5 2762.9	-1.97 -4.11	-4.98 -4.96	0493 1101	.0082 .0142	0059 0139	.0016 0003	0075 0074	.0259 .0262	0495 1109	.0065
.200 .201	2780.6 2790.0	02 1.88	-4.99 -5.00	0037 .0443	.0063	.0009	.0024	0077 0075	.0257	0037 .0445	.0063
.201 .200	2785.9 2775.0	3.86 5.79	-5.00	.1052	.0132 .0232	.0153	.0067	0079	.0252	.1059 .1721	.0061
. Z00	2776.8	7.78	-4.98	.2427	.0387	.0356	.0112	0095	.0266	.2457	.0055
.200 .200	2776.7 2770.4	9.84 11.81	-4.96 -4.94	.3241	.0612	.0490	.0135 .0155	0106 0120	.0264 .0272	.3297	.0050
.201	2804.6 2798.9	13.90	-4.91 -4.87	.4989	.1274 .1677	.0818	.0176 .0192	0136 0144	.0256 .0250	.5149	.003e
.200	2768.1 2786.9	17.93 19.29	-4.83 -4.79	.6804	.2225	.1187 .1318	.0213	0160 0164	.0169 .0141	.7159 .7858	.0022
.201	2785.1	.00	-4,99	0037	.0066	.0013	.0025	0078	0252	0037	.0066
			TEST 10	6		RUN 37					
HACH NUMB	9	ÅLPHA	BETA	CL	co	CHS	CRMS	CYMS	CYS	CN	CA
.200	2768.2	.03	9.00	.0034	.0064	\$200	0024	.0065	0241	.0035	.0064
.201 .200	2779.5 2764.4	-1.93 -4.24	5.00	0422	.0143	0045	0019	.0062 5000.	C247 O232	0424	.0058
.200 .201	2767.4 2791.9	1.93	5.00 4.98	.0020	.0063	.0019	0026	.0066	0244	.0020	.0063 .0062
.201	2800.7 2775.4	3.90	4.96	.1102	.0134	.0163	0062	.0072	0236 0244	.1109	.0059
.200 .200	2769.8 2778.3	7.83	4.91	. 2525	.0398	.0384	0102	.0085	0248 0231	.2556	.0050
.201	2781.3	9.89 11.87	4.87	.3319 .4168	.0626	.0518	C121 0138	.0099	0233	.3377	.0042
.200 .200	2750.6 2770.1	14.03 15.86	4.78 4.73	.5084	.1307 .1707	.0853 .1016	0155 0171	.0109 .0125	0225	.5250 .6146	.0035
.201 .200	2765.5 2773.8	17.95 19.30	4.67	.6879 .7471	.2248 .2628	.1219 .1346	0187 0197	.C145	0174 0152	.7237 .7919	.0018
.200	2771.8	.06	5.00	.0025	.0064	.0020	0027	.0063	0237	.0025	.0064
			TEST 10			RUN 49					
MACH Numb	PA	ALPHA Deg	BETA Deg	CL	CD	CHZ	CRMS	CYMS	CYS	CN	CA
.201 .201	2795.5 2795.2	.01 -1.94	00	.0081 0389	.0119 .0132	.0019	.0123 .0137	.0018	0056 0043	.0081 0393	.0119 .6119
.200	2777.1 2785.8	-3.80 00	.01	0963 0136	.0190 .0134	0077 .0063	.0136	.0021	0041 0022	0973 0136	.0126 .0134
.200	2776.3	1.87	01	.0690	.0158	.0041	.0133	.0008	0060	.0695	.G136
.201 .201	2793.4 2804.0	3.83 5.79	02	.1243	.0217 .0323	.0121 .0194	.0146	.0005	0071 0100	.1295	.0131
.201 .201	2792.7 2791.9	7.74 9.79	03 04	.2547 .3242	.0477 .0695	.0317	.0166	0007 000£	0087 0098	.2568 .3313	.0130
.200 .200	2785.0 2782.0	11.75 13.82	04	.4091	.0986	.0612 .0764	.0164	0012	0104	.4206 .5291	.0132 .0126
.200	2779.5	15.74	06 07	.586R .6753	.1761	.0950	.0147	0030	0091	.6131 .7129	.0123
.200 .200	2777.1 2780.6	17.80 19.37 01	07	.7471	.2738	.1173 .1325 .0005	.0149	0041	0103 0075	.7956	.0106
•	2,,,,,,	-102				RUN 50	*****			••••	****
	_	ALPHA	TEST . 10		C0		CRMS	CYMS	CYS	CN	CA
HACH NUMB	PA	DFG	BETA	CL		CMS					
.200 .200	2786.2 2780.0	.08 -1.90	00	.0443 0230	.0259	.0227 .0059	.0123 .0121	.0029	0053 0057	0238	.0259
.201 .200	2791.3 2790.0	-3.76 .07	.01 00	0732 .0540	.0262	0067	.0115	.0035	0056 0052	0745	.0214 .0260
.200 .201	2787.1 2793.5	1.96	01 02	.0995	.0330 .0427	.0295 .0395	.0117	.0027	0052	.1006 .1565	.0296
.201	2790.5	5.87	03	.2220	.0583	.0509	.0124	.0018 .	0051 0074	.2268	.0353
.200	2781.2 2787.7	7.84 9.91	03	. 3853	.1117	.0630	.0122	.0008	0096	.3987	.0437
.200	2784.8 2782.9	11.87 13.94	05 05	.4576 .5437	.1441	.0942 .1130	.0119	0020 0021	0052 0052	.4775 .5728	.0468
.201 .200	2807.1 2783.3	15.87 17.93	06	.6284 .7207	.2352 .2950	.130# .1512	.0126	0021 0016	0052 0074	.6688 .7765	.0544
.201 .201	2791.3 2803.5	19.48	07 00	.7871 .0429	.3437 .0272	.1681	.0142	0027 .0016	0105 0025	.8567	.0616
			TEST 100	4		RUN 51					
RACH		ALPHA	BETA	CL	CD	CHS	CRMS	CYMS	CYS	CN	CA
NUM8 • 201	2790.8	0EG •10	0EG	.0379	.0311	.0356	.0016	0001	0013	.0380	.0310
.200 .200	2771.9 2779.9	-1.89 -4.14	.01 .02	0378 1021	.0283 .0307	.0152 .0003	.6002	0004 cool	0020 0016	0387 1040	.0271
.201 .200	2791.7 2781.3	.11 2.02	.00 01	.0446	.0310	.0330	.0010	0004	0020 0013	.0446	.0309
.201 .201	2790.3	3.96 5.90	02	.1463	.0469	.0567	.0003	0002 0011	0031 0029	.1493 .2067	.0387
. 200	2783.6	7.88	03	.2668	.0847	.0779	.0009	0019	0022	.2759	.0473
.200 .200	2774.3 2780.7	9,93	04	.3495	.1142 .1495	.0910	.0007	0004	0054	.3640	.0522
.201 .201	2798.6 2803.5	13.97 15.89	06 07	.5080	.1902 .2361	.1264 .1440	.0024	0005 0013	0054	.5369	.0619
.201	2809.5 2787.1	17.95 19.29	08	.6790	.2946	.1629 .1759	.0019	0010 0018	0056	.7368	.0710
.201	2794.0	•11	.00	.0394	.0317	.0335	.0016	0008	0036	.0395	.0316

TABLE II. continued

			NASA LANGLEY		7 X 10 HIGH SPEED TUNN				MEL		
			TEST 10	6		RUN 52					
MACH	0 PA	ALPHA	BETA DEG	CL	CD	CHS	CRMS	CYMS	CA2	CH	CA
.201	2794.7 2785.0	DEG -11	.00	.0343 0291	.0501	.0466	.0002	0007 0008	.0004	.0344 0306	.0501 .0458
.200	2776.2	-1.06 -4.39	.02	1000	.0484	.0129	0001 .0007	0005	.0001	1034	.0406
.200	2793.6 2784.1	2.07	.00 01	.0387	.0506	.0475 .0621	.0005	0013	0005	.0388	.0505
.201 .200	2789.5 2783.6	5.93	01 02	.1591	.0715	.0734	.0008	0019	0013 0015	.1637 .2215	.0646
.201	2794.5 2794.9	7.91 9.95	03	.2781	.1085	.0916 .1024	.0007	0007 0011	0007	.2904 .3644	.0692 .0743
.200	2779.3	11.70	05	.4184	.1696	.1149	.0009	0017 0016	0034 0035	.4444	.0796
.201 .200	2791.3 2789.5	13.96 15.87	06	.4995	.2120 .2579	.1285 .1430	.0011	0021	0042	.5358 .6237	.0852
.201	2788.2 2790.7	17.93 19.35	08	6636	.3170	.1599 .1716	.0014	0017	0027 0030	.7290 .7988	.0973
.201	2795.0	.12	.00	.0337	.0522	-0470	.0004	0002	.0004	.0336	.0521
			TEST 10	6		RUN 53					
MACH NUMB	Q PA	ALPHA DEG	BETA DFG.	CL	CD	CHS	CRMS	CYMS	CYS	CH	CA
.200	2764.4	.00	00	.0006	.0124	0020	.0028	.0013	0044	.00P7	.0124
.200	2768.8 2769.5	-1.93 -4.37	•01 •02	0447 1175	.0141	0063 0163	.0014	0000	0018	0451 1189	.0126 .0137
.200 .201	2780.9 2795.1	1.90	00 01	.0019	.C115	0016 50052	.0016	.0005	0021 0027	.0019	.0115 .C104
.201	2795.6 2782.3	3.87 5.83	02	.1159	.0172	.0127 .0184	.0008	.0001 .CC01	0022	.1164	.0094
.200	2777.6	7.76	04	.2560	.0420	.0250	.0002	0002	0010	.2593	.0070
.200	2773.9 2778.8	9.91 11.77	04	.3277	.0620	.0369 .0492	.0010	000Z 0007	0020	.3335	.005Z
.201	2792.2 2771.9	13.86 15.72	06	.4982	.1244	.0667 .0821	.0017	0004	0015	.5135	.0014
.200	2765.8	17.78	08	.6759	.2132	.1015	.0013	0006	0006	.7087 .7916	0034 0058
.200	2779.3 2780.3	19.31	08	.7490	.2564	0035	.0009	0005	0016	.0097	.0122
			TEST 10	6		RUN 54					
MACH	0	ALPHA	BETA	CL	CD	CHS	CRMS	CYMS	CYS	CN	CA
.201	2707.5	DEG 03	00	0099	.0181	0134	.0016	.0007	.0006	0100	.0191
.200	2768.4 2760.3	-2.03 -4.58	.01 .02	0605 1394	.0230	0242 0366	.0012	0001 0004	0005	0613 1418	.0208 .0252
.201	2790.3	04	00	0106	.0181	0139 000Z	.0018	.0003 0003	0014	0106	.0181 .0163
.201	2802.3 2789.4	1.86 3.83	01 02	.1106	.0209	.0105	.0015	0064	*000Z	.1116	.0135
.200	2775.1 2774.9	5.80 7.72	03 04	.1770 .2467	.0291	.0169 5850.	.0017	6003	0002	.1791 .2501	.0110
.200	2767.4 2783.1	9.75 11.76	04	.3166	.0595	.0365	.0015	0002	.0003	.3240	.0047 .0017
.201	2792.1	13.75	06	. 4 6 4 4	.1177	.0612	.0018	.000	.0005	.4985	0008
.200	2767.2 2793.7	15.67 17.72	07	.5700	.1561	.0751 .0911	.0021	CC10	.0007	.5910 .6946	0037
.201 .201	2788.8 2786.0	19.20 05	09	.7343 0111	.2451 .0184	.1040 0139	.0016	0004	0000	.7741 0111	01C0 -0184
			TEST 10	6		RUN 55					
MACH	9	ALPHA	BETA	CL	CO	CMS	CRMS	CYMS	CYS	CN	CA
.200	9 PA 2776.5	0 E G • 0 1	DFG 00	.0033	.0082	.0034	.0016	.0007	.0001	.0033	.0082
.201	2789.6 2772.2	1.90	01 .01	.0551 0433	.0099	0025	.0024	.0003	.0005	0437	.0081
.201	2787.1	-4.42	.02	1185	.0186	0124	.0018	.0005	0000	1195	.0094
.201	2791.2 2793.3	1.90	00 01	.0058 .0572	.0102	.0036	.0020	.0005	.0003	.0575	.0083
.201 .200	2792.0 2775.6	3.86 5.82	02	.1144	.0152 .0247	.0153 .0221	.0018	cooo cool	0000	.1152 .1777	.0068
.200	2768.6 2761.9	7.75 9.81	04	.2478 .3274	.0396	.0321	.0022	0001	0000	.2509 .3331	.0058
.201	2797.7	11.76	05	.4085	.0887	.0560	.0020	0000	.6005	.4180	.0035
.200	2770.2 2772.2	13.98 15.76	06 07	.5066	.1283 .1677	.0759 .0916	.0020	0006	.0015	.5276 .6149	.0007
.200	2773.8 2785.9	17.81 19.32	08	.6872 .7593	.2200 .2634	.1102 .1269	.0013	0006 0001	.0025	.7216 .8037	0008
.255	2778.7	.01	03	.0139	.0096	.0016	.0015	.0003	.0013	.0139	.0096
			TEST 10	6		RUN 56					
MACH NUMB	Q PA	ALPHA DEG	BETA DEG-	CL	CD	CMS	CRMS	CAW2	CYS	CH	CA
.201	2796.6 2783.9	01 -1.95	-5.01 -4.99	.0065 0420	.0057	.0009 0072	.0014	.0022	.0050	.0065	.0057
.200	2773.6	-4.29	-4.97	1116	.0137	0162	0025	.0016	.0053	1123	.0053
.201 .201	2799.5 2800.5	.03 1.58	-5.01 -5.01	.0052 .0552	.0058	.0004	.0011	.0021	.0046	.0052 .0554	.0058
.201	2000.2 2780.5	3.59 5.80	-5.01 -5.00	.1151	.0135 .0237	.0142	.0064	.0015	.0039	.1158	.0056
.201	2788.8 2785.0	7.84 9.85	-4.99 -4.97	.2562	.0403	.0359	.0117	0002	.0046	.2593	.0050
.200	2777.6	11.60	-4.95	.4154	.0912	.0643	.6162	0025	.0053	.4253	.0044
.200 .201	2778.4 2792.6	13.87	-4.92 -4.88	.5041 .5934	.1203 .1714	.0912	.0182	0056	.0041	.5201	.0037
.200 .201	2777.7 2795.9	17.90 19.48	-4.84 -4.80	.6868 .7614	.2241 .2706	.1193 .1359	.0223	0080	0016	.7224	.0021
,201	2792.6	.02	-5.00	.0078	.0060	.0000	.0017	.0021	.0041	.0076	.0060

TABLE II. Concluded.

		MASA LANGLEY				7 x 10 HIGH SPEED TUNNEL						
			T65T 10	6		RUN 57						
MACH	. •	ALPHA	BETA	CL	CD	CMS	CRMS	CYMS	CYS	CM	CA	
MURB		DEG	DEG	4174			.0024	.0009	.0021	.0178		
.200	2786.7	.04	-5.00 -4.99	.0178	.0178 .0162	.0214 .0079	.0001	.0010	.0030	0398	.0178 .0149	
•200 •199	2778.6 2757.4	-1.95 -4.17	-4.97	039Z 1039	.0188	0050	0026	.0008	.0035	1050	.0112	
.201	2791.9	.03	-5.00	.0203	.0178	.0214	.0028	.0008	.0019	.0203	.0175	
.201	2796.6	1.91	-5.01	.0762	.0230	.0337	.0050	.0003	.0002	.0769	.0205	
.200	2788.5	3.88	-5.01	.1316	.0323	.0441	.0081	0006	0032	.1335	.0233	
.200	2780.1	5.87	-5.00	.1944	.0466	.0553	.0117	0021	0058	.1981	.0265	
.200	2787.3	7.87	-4.98	.2669	.0682	.0701	.0115	0048	0053	.2737	.0310	
.200	2786.6	9.94	-4.96	.3555	.0979	.0866	.0150	0073	0035	.3671	.0351	
.200	2770.8	11.90	-4.93	.4289	.1294	.1015	.0167	0092	0066	.4464	.0382	
200	2773.0	13.94	-4.90	.5129	.1707	.1202	.0183	0110	0087	.5389	.0422	
-200	2775.6	15.87	-4.86	.5950	.2167	.1377	.0205	0132	0120	.6316	.0457	
.201	2799.6	17.95	-4.82	.6853	.2740	.1574	.0227	0162	0167	.7364	.0495	
105.	2789.6	19.32	-4.76	.7393	.3143	1703	.0230	0180	0200	.8017	.0520	
.201	2797.9	.03	-5.00	.0188	.0182	.0218	.0027	.0006	.0019	.0148	.0182	
			TEST 10	6		RUN 58						
MACH	٥	ALPHA	BETA	CL	CO	CAS	CRMS	CYMS	CYS	CH	CA	
NURS	PĀ	DEG	DEG				•	• • • • • • • • • • • • • • • • • • • •		• •	•	
.201	2798.0	.08	5.00	.0210	.0181	.0228	0020	0008	0031	.0210	.0181	
.200	2781.6	-1.92	5.01	0346	.0166	.0102	0001	0007	0025	0352	.0154	
.201	2797.1	-4.30	5.01	1078	.0169	0046	.0030	6007	0030	1090	.0107	
. 200	2787.9	.09	5.00	.0227	.0181	.0227	0020	0006	0022	.0227	.0181	
.201	2002.3	1.75	4.99	.0765	.0236	.0351	0037	0002	0018	.0773	.0210	
.201	2800.4	4.00	4.97	.1348	.0332	.0455	0072	.0010	.0024	.1368	.0237	
.201	2792.4	5,92	4.94	.1992	.0480	.0577	0103	.0025	.0045	.2031	.0272	
.200	2784.6	7.90	4.91	.2745	.0700	.0720	0107	.0050	.0021	.2816	.0317	
.201	2797.9	9.96	4.87	.3561	.0986	.0877	0134	.0067	.0017	.3678	.0355	
.201	2790.6	11.97	4.83	. 4365	.1325	.1644	0150	.0083	.0038	.4545	.0390	
.200	2774.7	14.01	4.78	. 5253	.1750	.1220	0177	.0103	.0058	.5521	.0425	
.200	2766.2	15.98	4.72	.6071	.2217	.1402	0192	.0122	.0092	.6447	.0460	
.200	2770.4	17.99	4.66	.6917	.2768	.1595	0207	.0147	.0132	.7433	.0496	
.201	2790.2	19.50	4.61	.7532	.3225	.1740	0212	.0164	.0165	.8176	.0526	
.201	2806.5	.10	5.00	.0239	.0186	.0234	-•00ŠS	0006	0023	.0239	.0186	
			TEST 10			RUN 59					·	
MACH	. 0	ALPHA	BETA	CL	CD	CAS	CRMS	CYMS	CYS	CH	CA	
NUMB	PA	DEG	DEG									
.201	2788.7	.03	5.00	•0072	.0057	.0015	0008	0016	0048	.0073	.0057	
.201	2700.6	-1.89	9.01	0363	.0067	0056	0002	0020	0055	0365	.0055	
. 200	2774.8	-4.45	5.01	1175	.0141	0173	.0031	0010	0045	1162	.0044	
.200	2775.5	.03	5.00	.0060	.0055	.0009	0010	C019	0052	.0060	.0055	
. 201	2787.8	1.94	4.99	.0581	.0076	.0070	0034	0016	0045	.0363	.0057	
.201	2794.3	3.94	4.97	.1215	.0137	.0162	0053	0011	0045	.1221	.0033	
.201	2792.8	5.90	4.95	. 1856	.0241	.0249	0083	6006	0052	.1671	.0049	
.201	2785.9	7.82	4.92	.2600	.0404	.0374	0162	.0004	0645	.2631	.0047	
.201	2797.0	9.60	4.88	.3372	.0629	.0501	0128	.0012	0058	.3430	.0041	
.201	2786.7	11.86	4.84	.4204	.0920	.0652	0150	.0023	0064	.4303	.0036	
.200	2769.2	13.99	4.79	.5138	.1311	.3841	0165	.0038	0056	.5303	.0030	
.200	2770.6	15.90	4.74	.5993	.1730	.1004	0186	-0057	0037	.6237	.0022	
.200	2771.8	17.94	4.68	.6915	.2252	.1205	0204	.0080	0009	.7273	.0013	
.200	2777.8	19.40	4 - 6 2	.7686	.2740	.1375	0218	.0095	.0004	.6159	.0002	
.200	2772.5	.04	5.00	.0076	.0056	.0014	0010	0019	0053	.0076	.0056	

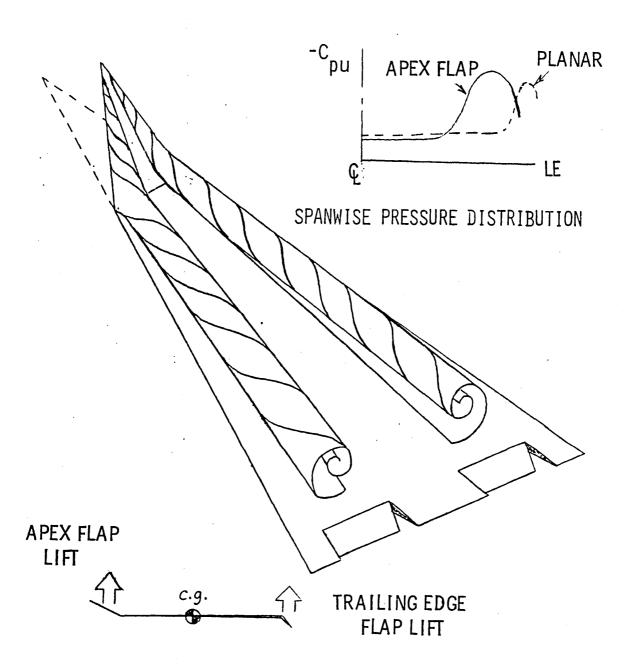


Figure 1.- Apex Flap Concept.

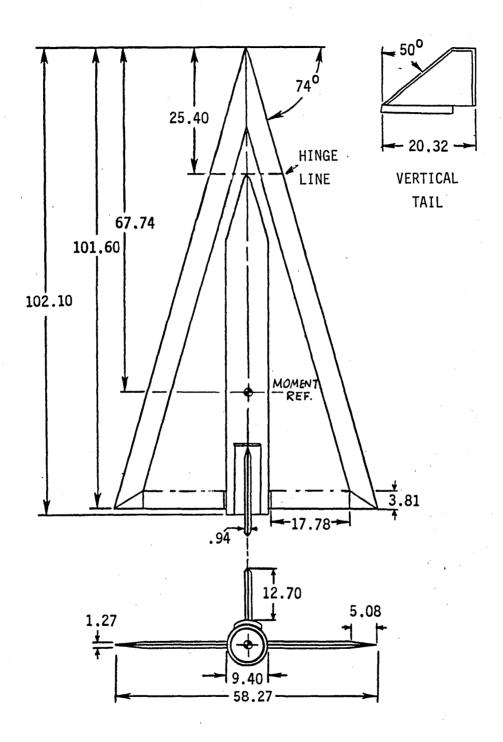


Figure 2.- 74<sup>0</sup> Delta Model. Dimensions in centimeters.

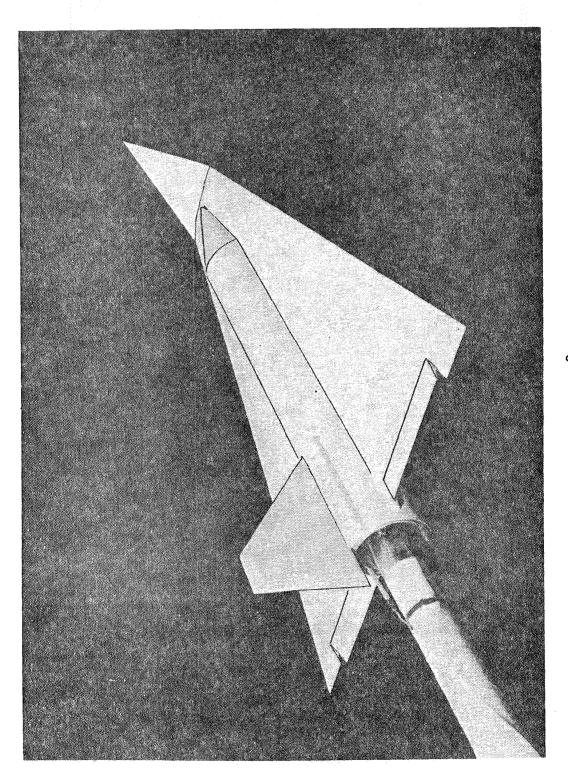


Figure 3.- NASA 74° Delta Wing.

1. Report No. NASA CR-166081	2. Government Acces	ision No.	3. Rec	ipient's Catalog No.	
4. Title and Subtitle			5. Report Date		
Force and Moment Measurements on a 74° Delt With an Apex Flap (Data Report)			Wina	October 1984	
			6. Perf	6. Performing Organization Code 505-31-43-03	
7. Author(s)			8. Perf	orming Organization Report No.	
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North Carolina State University			11. Contract or Grant No.		
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12. Sponsoring Agency Name and Address					
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Washington, DC 2054		14. 300	505-31-43-03		
15. Supplementary Notes				505-51-45-05	
*North Carolina State University, Raleigh, NC 27650					
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**Vigyan Research Associates, Inc., 28 Research Drive, Hampton, VA 23666 Langley Technical Monitor: W. E. Schoonover, Jr.					
16. Abstract					
Results are presented of a subsonic experimental investigation of an apex flap concept on a 74° swept delta wing with trailing-edge flaps. The apex flap comprised approximately 6 percent of the wing area forward of a transverse hinge, allowing for both upward and downward deflection angles from +40° to -20°. Upward deflection forces leading-edge vortex formation on the apex flap, resulting in an increased lift component on the apex area. The associated nose-up moment balances the nose-down moment due to trailing-edge flaps, resulting in sizeable increase in the trimmed lift coefficient particularly at low angles of attack. Nose-down apex deflection may be used to augment the pitch control for rapid recovery from high-alpha maneuvers. Balance measurements were obtained in the NASA Langley 7- by 10-Foot High-Speed Tunnel at M <sub>∞</sub> = 0.2 and R <sub>c</sub> = 4 x 10°. This report presents the balance data without analysis.					
17. Key Words (Suggested by Author(s))  18. Distribution Statement					
Apex flap					
Balance measurements		Unclassified - Unlimited			
Trimmed lift Vortex lift					
10.00%			Subject Category 02		
19. Security Classif, (of this report)	20. Security Classif, (of this	nage)	21. No. of Pages	22. Price	
Unclassified	Unclassifi	-	22	A02	
Unclassified	Unclassifi	cu			

**End of Document**